

## Current characteristics of the present RAFAEL E-gun

In the space charge limited operating regime the electron gun maximal current is:

$$J_0 = 2.33 \cdot 10^{-6} \frac{V_0^{3/2}}{d^2} [A/m^2] \quad (1)$$

Where:  $V_0$ -Grid potential [volt]

$d$  – distance from cathode to grid[m]

This equation is well-known Child-Langmuir law.

The cathode current:

$$I = \pi r^2 \cdot J_0 [A] = 2.33 \cdot 10^{-6} \pi r^2 \frac{V_g^{3/2}}{d^2} [A] \quad (2)$$

Where:  $r$  – cathode radius

In the present gun:  $d=17\text{mm}$  – distance from cathode to grid

$r=7.5\text{mm}$

$V_g = 6 - 20\text{kV}$  – grid potential

and therefore the current:

$$I = 1.421 \cdot 10^{-6} \cdot V_g^{3/2} [A] \quad (3)$$

Fig1. displays data characteristics of  $I_c=I_c(V_g)$  obtained in three different ways:

1. The Child-Langmuir law (Eq.3).
2. “E-GUN” simulations carried out for different values of  $V_g$  for a fixed anode – cathode voltage  $V_{ac}=45$  kV.
3. Experiments carried out by Yoram Lasser 31.10.02 (after the e-gun was cleaned and reassembled on the accelerator) the cathode. The cathode used was a new cathode model STD 600 M-type (0.6” diameter). Experiment with different cathode temperatures and different  $V_{ac}=40,45,50$  kV, are plotted. The gun was pulsed with the “Old Haim Pulser” which was operated with pulse duration  $t_p=13\mu s$  and blocking voltage  $V_g=-2$  kV. It is important to note that  $V_g$  is the “real value on the grid. It was obtained from the voltage read from the LABVIEW control program, by use of a “calibration cure”, in order to take into consideration voltage drops on resistors and capacitors in the grid pulsing circuit.

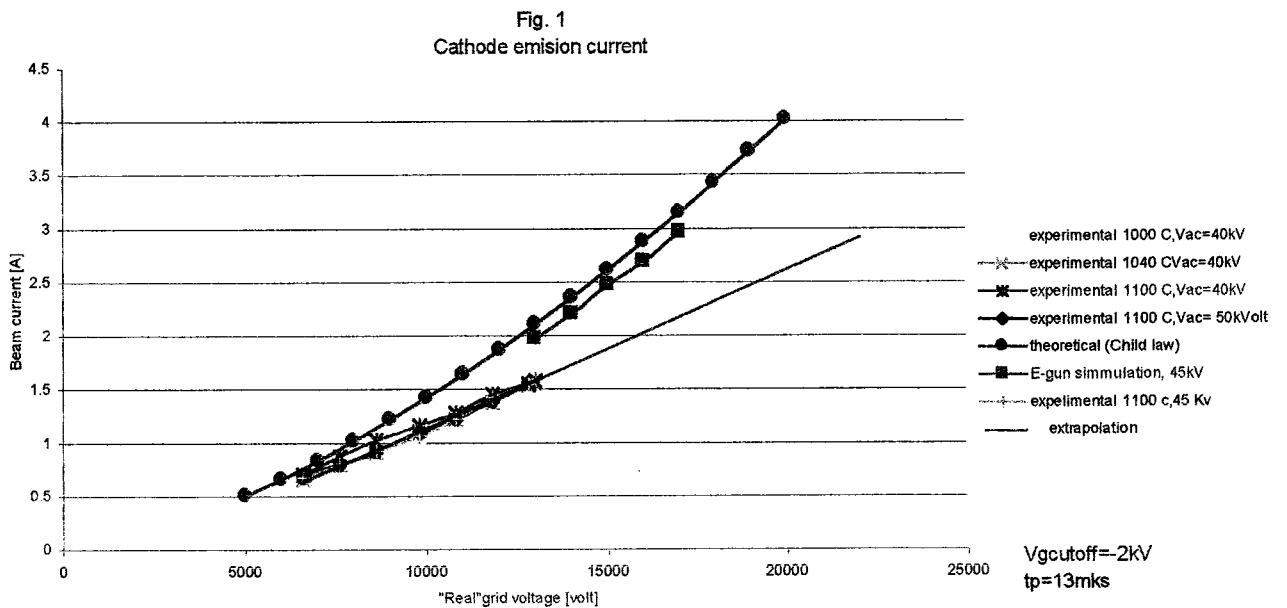
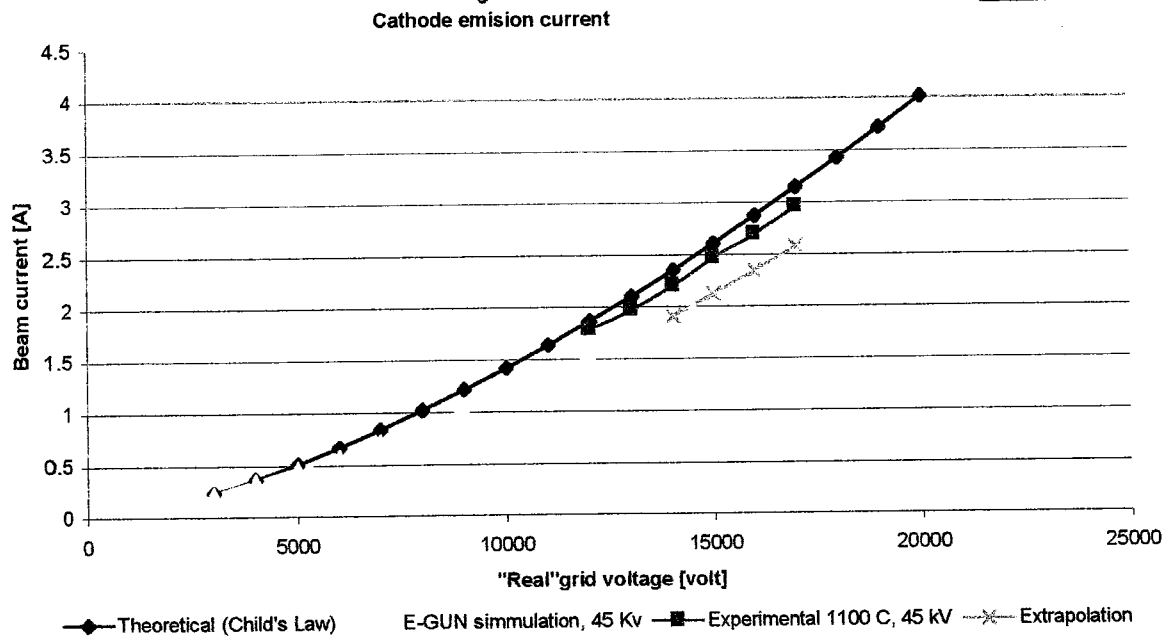


Fig. 2a,b. displays data characteristics of  $I_c = I_c(V_g)$  obtained in the same three ways, with “New Haim Pulser”

Vac=40 kV, Vgcutoff=-2kV, tp=12mks

Fig. 2a

03.12.02



Vac=40 kV, Vgcutoff=-2kV, tp=12mks

Fig.2b

Cathode emission current, Logarithmic scale (New pulser)

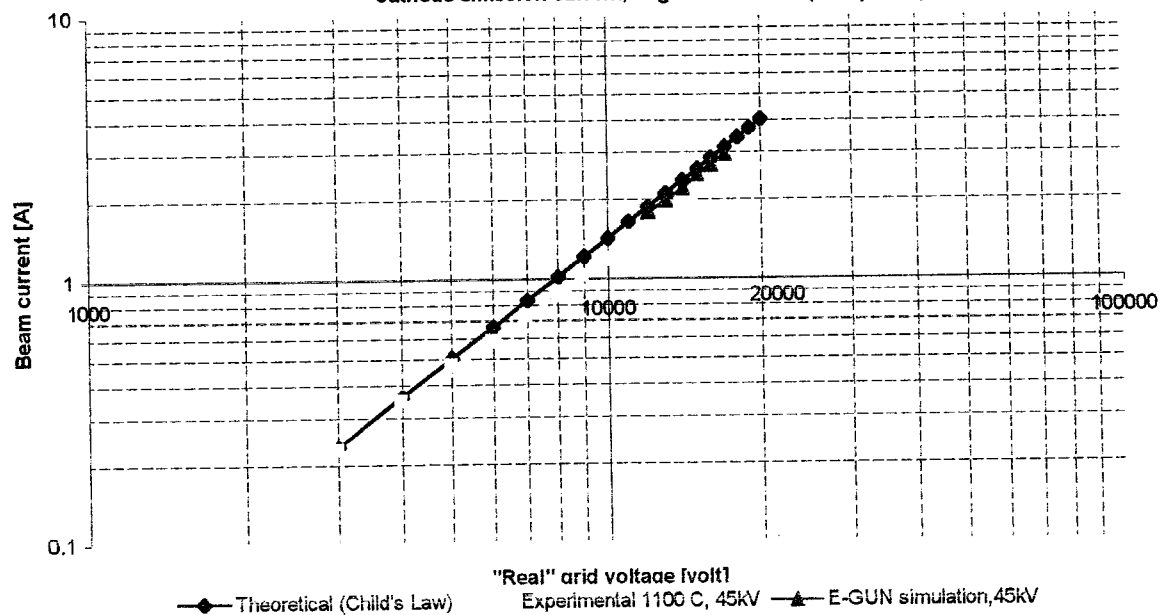


Fig.3 displays “E-gun” trajectories of the electron – gun in the “space charge limited regime” for  $V_{ac}=45\text{kV}$  and two values of  $V_g=12,17\text{ kV}$ .

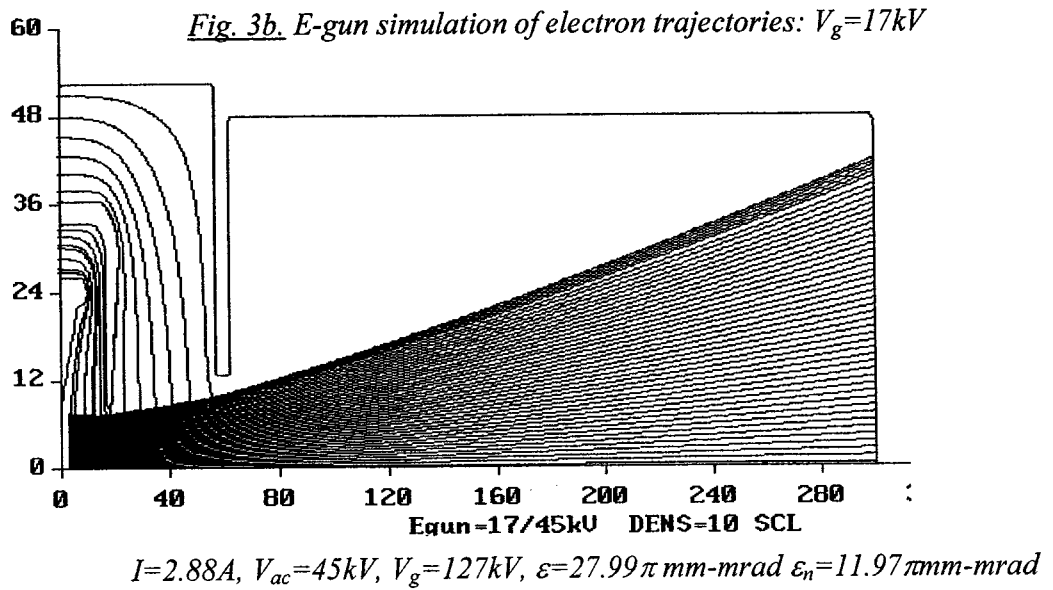
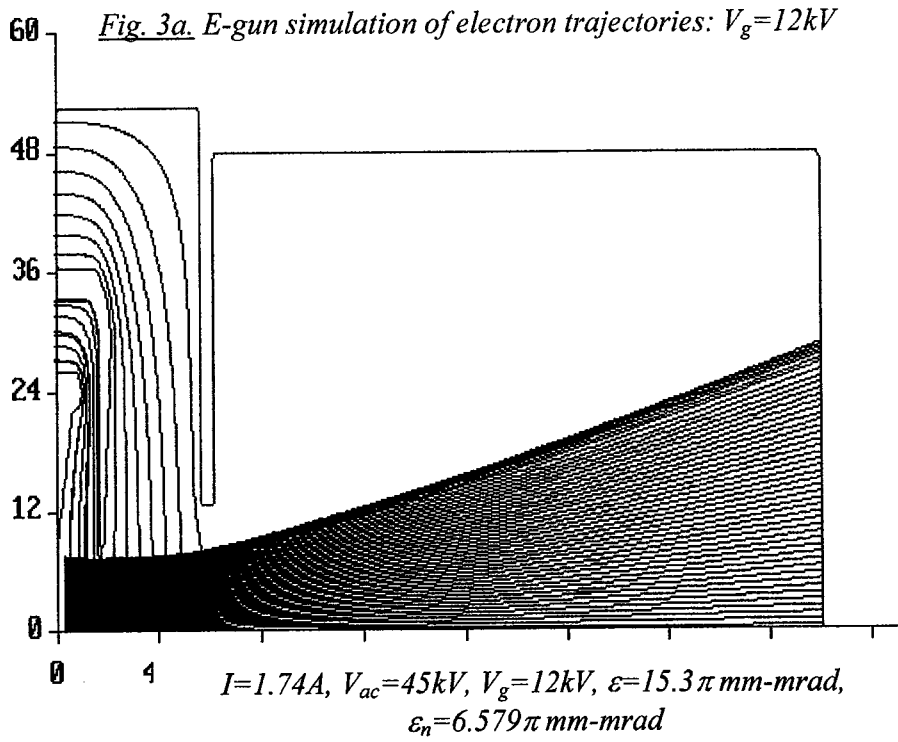


Fig.4 and Fig.5 display the current density distribution and the phase space distribution of the accelerated beam in these two cases of  $V_g = 12, 17\text{kV}$

Fig.6 shows the increase in emittance as a function of  $V_g$  for fixed  $V_{ac} = 45\text{kV}$ .

*Fig.4: The current distribution and phase – space distribution of the e – beam for  $V_g = 12\text{kV}$ ,  $V_{ac} = 45\text{kV}$*

*Fig.4a*

**I = 1.746 AMPS, PERVEANCE = .1829 MICROPERVS  
EMITTANCE = 15.39 PI (MM-MR)  
NORMALIZED EMITTANCE = 6.579 PI (MM-MR)**

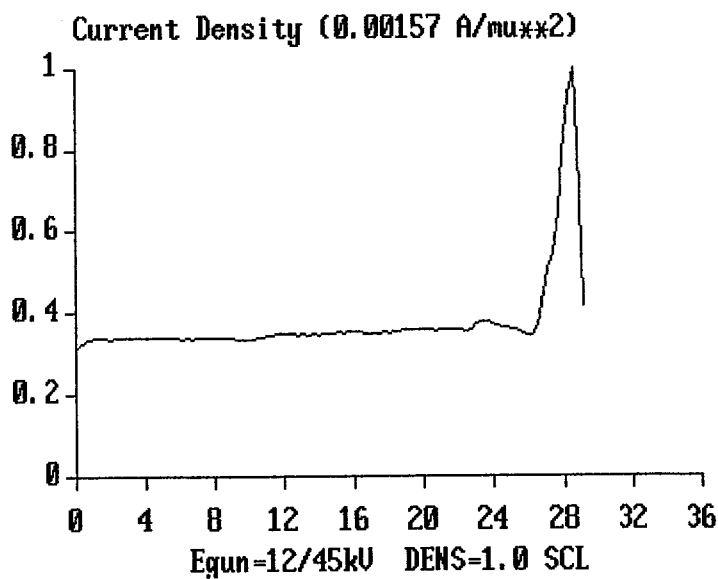


Fig.4b

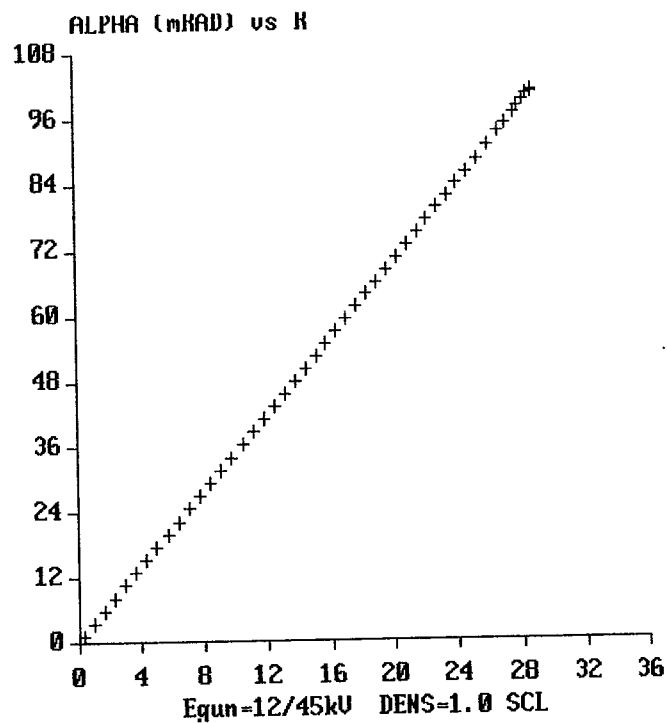


Fig. 5: The current distribution and phase – space distribution of the e–  
beam for  $V_g = 17kV$ ,  $V_{ac} = 45kV$

Fig.5a

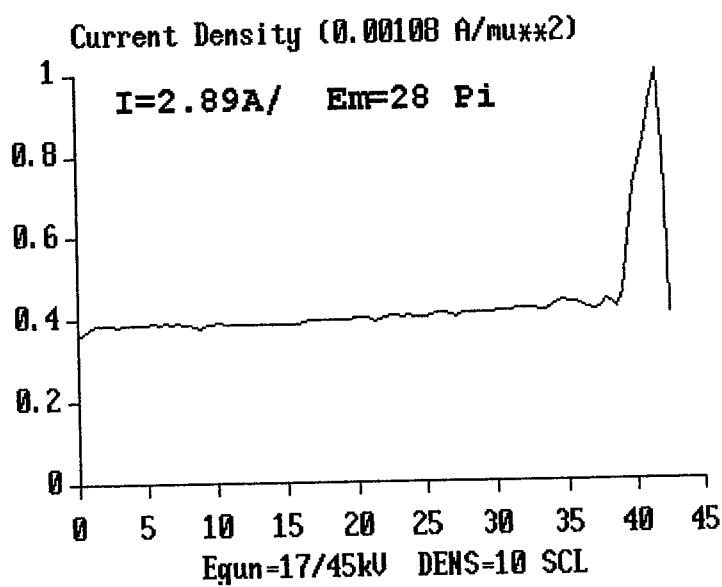


Fig.5b

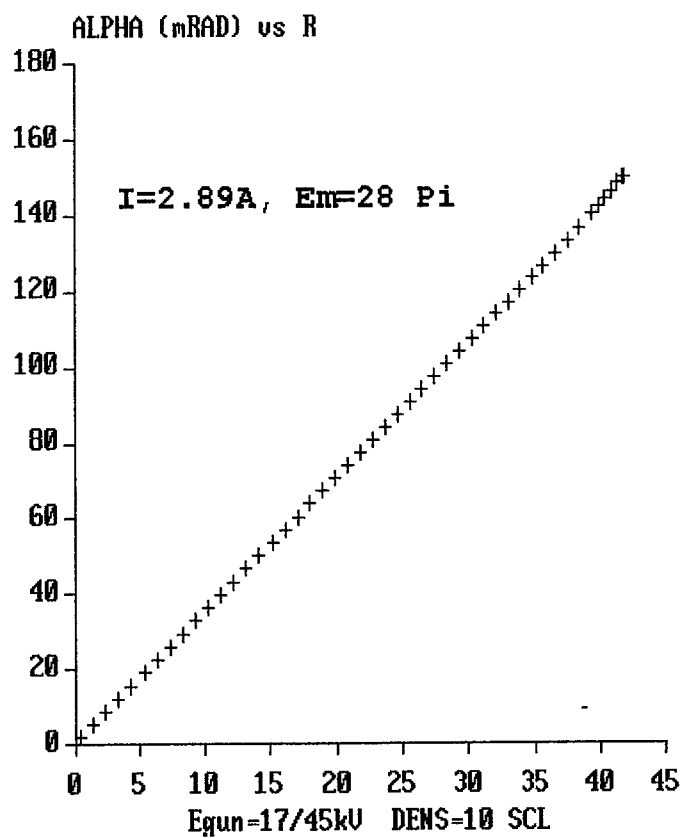
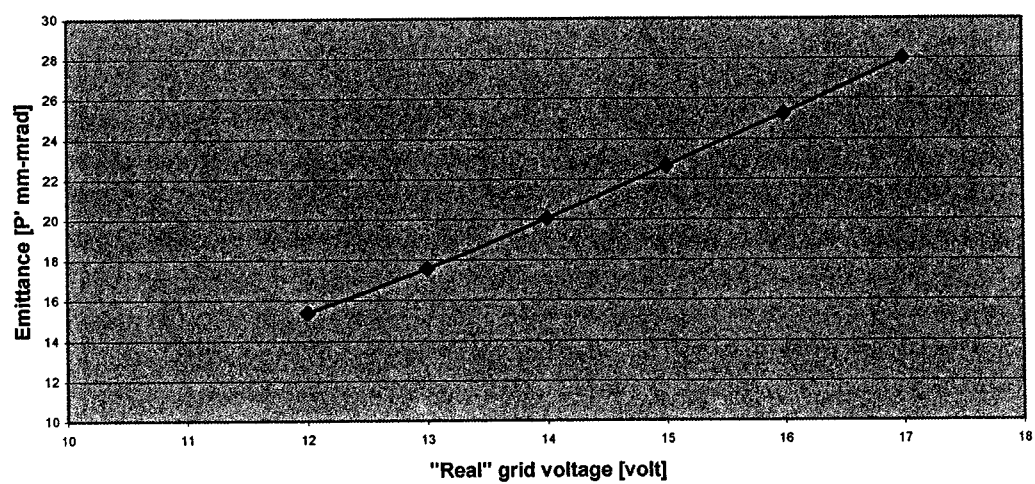


Fig. 6 Results of E-gun simulation



## Observations

1. The E-GUN simulations of  $I_c(V_g)$  (Fig.1,2) is a little lower but close to Child-Langmuir law (Eq.3). The experimental results are significantly lower than both predictions. A possible explanation: the grid-cathode spacing is in reality longer than 17mm (e.g.-because flanges were not tightened face to face – 22mm!).

An important observation is that the experimental curves for different  $V_{ac}$  are not really different, so that as far as the current parameter is concerned the grid operates well as a current control in the range 6 – 13kV (independent of  $V_{ac}$ ).

The weak dependence on cathode temperature indicates that the operation in all cases is in the space – charge regime.

2. While the grid operates well as a current control, it is known that when its voltage varies too much relative to a nominal voltage, it may cause defocusing effect and possibly emittance growth. Comparison of trajectories for  $V_g=12kV$ , 17kV (Fig. 3a,b) reveals bigger expansion in the latter case, but this can be attributed also to the space – charge effect at the larger current ( $I_c=2.69A$  increased of  $I_c=1.746A$ ).

Figs.4, 5 show, that the emittance in the case of  $V_g=17kV$  ( $\epsilon=27.99\pi$  mm-mrad,  $\epsilon_n=11.97\pi$  mm-mrad) is larger than the emittance of  $V_g=12kV$  ( $\epsilon=15.39\pi$  mm-mrad,  $\epsilon_n=6.579\pi$  mm-mrad) by a significant factor:  $\times 1.82$ . This can be attributed also to the increase in current (according to Lawson – Penner law  $\epsilon \propto \sqrt{I_c}$ , which would account for a factor of  $\times 1.31$ )



Fig.6 indicates that the increase of emittance as a function of  $V_g$  is monotonic and nearly linear.

3. According to the C-L law (in 1D model!), in order to get transversely uniform potential in the grid region (to avoid focusing effect) one needs to satisfy:

$$\frac{V_g^{3/2}}{d_g^2} = \frac{V_{ac}^{3/2}}{d_a^2}$$

This ratio gives for  $V_{ac}=45\text{kV}$   $d_g=17\text{mm}$ ,  $d_a=57.5\text{mm}$

$$(V_g)_{\text{opt}}=8.87\text{kV}$$

or alternatively, for  $V_g=12\text{kV}$

$$(V_a)_{\text{opt}}=60.9\text{kV}$$

Because of these considerations we ran E – GUN also for  $V_{ac}=60\text{kV}$ ,  $V_g=12,17\text{kV}$  (Figs. 7, 8). Fig.6a shows nearly uniform flow from the cathode to the anode, however there is slight focusing effect, which should be attributed to the deviation from the 1D model of the C-L law. Fig.8a displays some expansion of the beam (under-focusing) between the cathode and anode, but the beam is still quite uniform.

Fig.7 E-GUN simulation for  $V_g=12\text{kV}$ ,  $V_{ac}=60\text{kV}$  (optimal case):  
 (a)trajectories, (b)current distribution, (c)phase space diagram.

$I= 1.7840\text{ A}$ , PERVEANCE = .12139 MICROPERVS  
 EMITTANCE =11.37 PI(MM-MR) FROM 48 RAYS  
 NORMALIZED EMITTANCE =5.644PI(MM-MR)  
 Average current density= $0.00909\text{ A/mm}^2$

Fig.7a

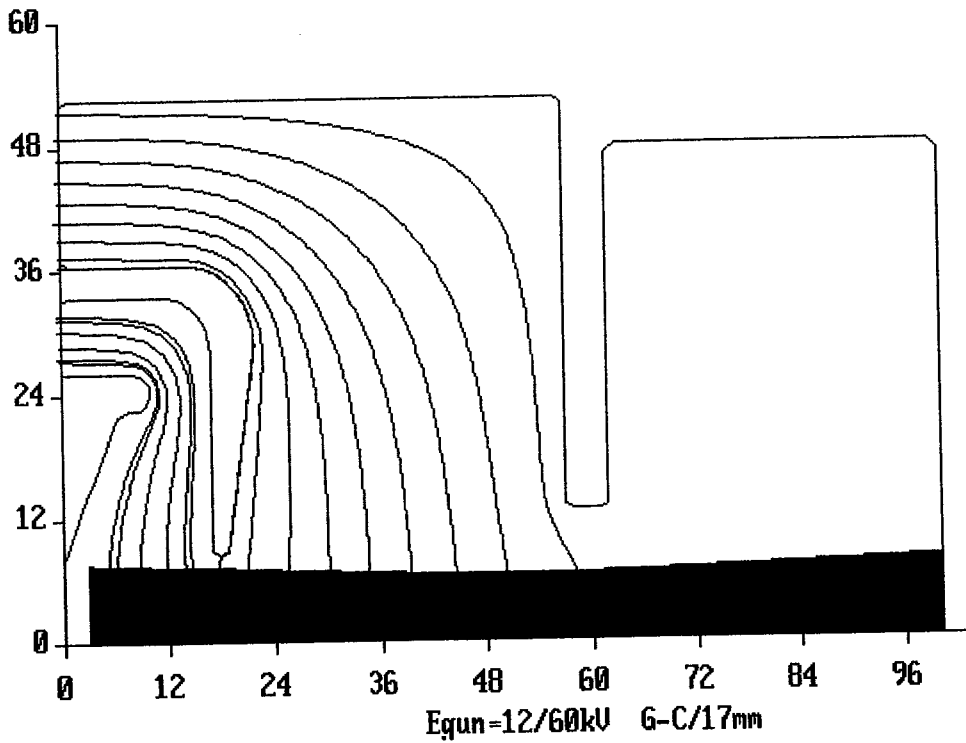


Fig.7b

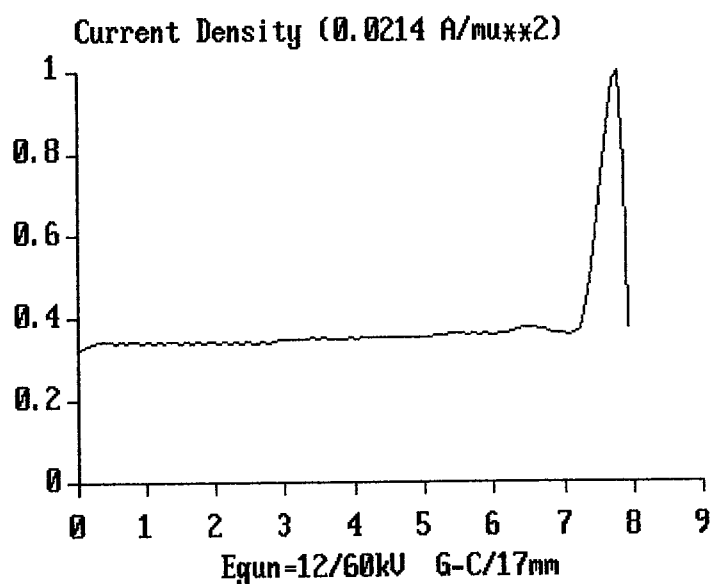


Fig.7c

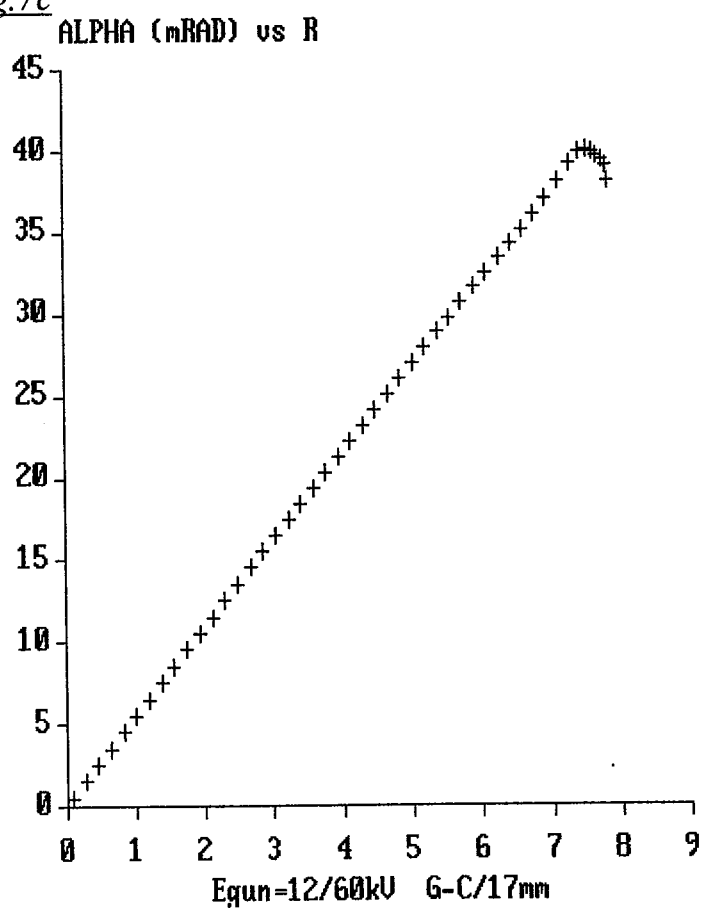


Fig.8 E-GUN simulation for  $V_g=17kV$ ,  $V_{ac}=60kV$  (optimal case):  
 (a)trajectories,(b)current distribution, (c)phase space diagram.

$I= 2.9312 A$ , PERVEANCE = .19944 MICROPERVS  
 EMITTANCE =12.10 PI(MM-MR) FROM 48 RAYS  
 NORMALIZED EMITTANCE =5.997 PI(MM-MR)

Fig.8a

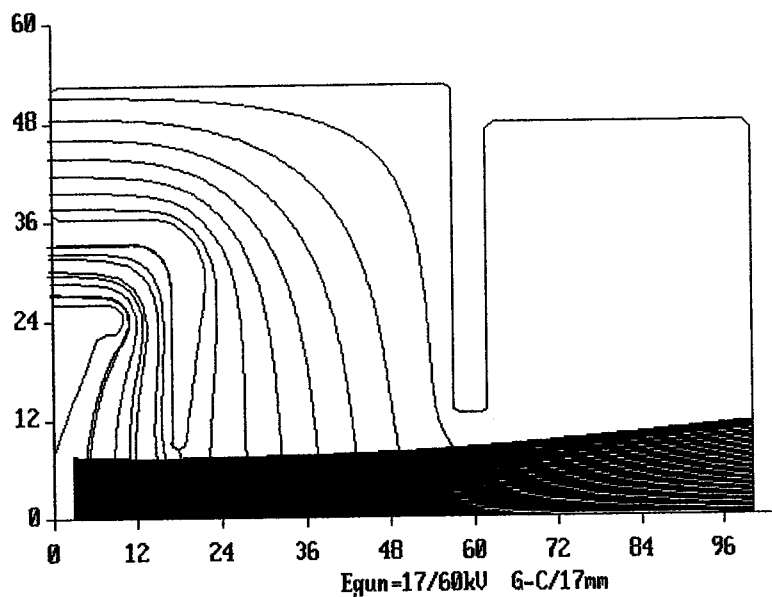
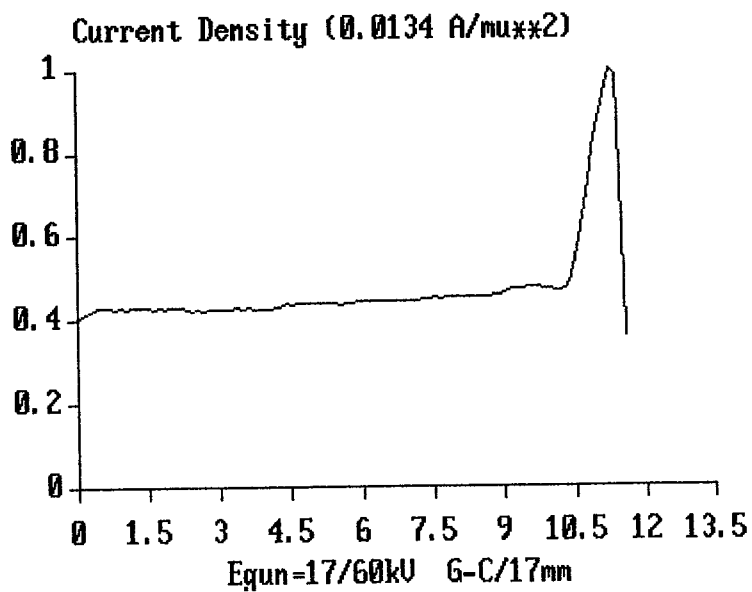
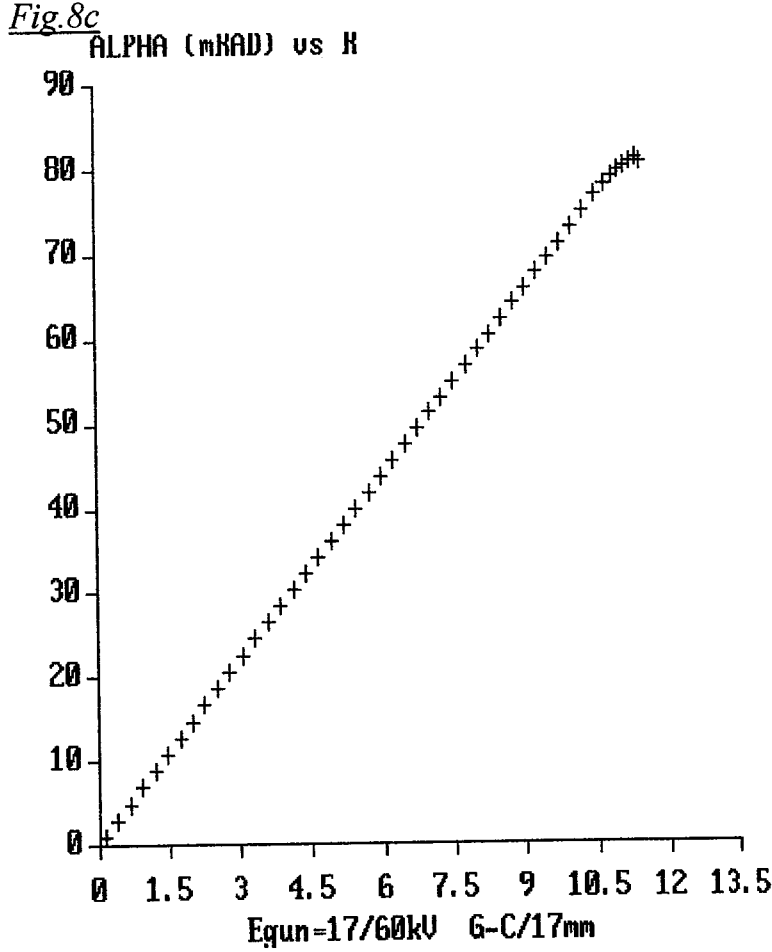


Fig.8b





The normalized emittance of ( $V_g=12\text{kV}$ ,  $V_{ac}=60\text{kV}$ ):  $\epsilon_n=5.6\pi$  mm-mrad is better in this “optimal case than the normalized emittance of ( $V_g=12\text{kV}$ ,  $V_{ac}=45\text{kV}$ ):  $\epsilon_n=6.58\pi$  mm-mrad (note that the currents are about the same  $I_c=1.75\text{A}$ ). However in the case of  $V_{ac}=60$  kV, even when we increase the grid voltage to  $V_g=17\text{kV}$ (fig7.), increasing the current significantly to  $I_c=2.93\text{A}$ , the normalized emittance only slightly increases (from  $\epsilon_n=5.6\pi$  mm-mrad to  $\epsilon_n=6\pi$  mm-mrad). This should be compared to the large increase in normalized emittance (factor of  $\times 1.8$ ) when we change  $V_g=12\text{kV}$  to  $17\text{kV}$  for  $V_{ac}=45\text{kV}$ .